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**CONTROLLED-RUPTURE DEVICE FOR A STRUCTURE OPERATING IN
TENSION AND EQUIPMENT USING THE SAME**

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15 More specifically still, the present invention
preferably applies to the field of assemblies
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25 In particular, numerous rupture devices based on
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On this point, reference may be made, for example, to
documents FR-A-2 495 991, FR-A-2 492 336,
FR-A-2 364 746, FR-A-2 464 778 and EP-A-55165.

30 These known devices are still not satisfactory,
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10 However, hitherto, the devices of this type have still not been satisfactory either. They also lead to not insignificant shocks and to risks of pollution following the escape of the gases originating from the pyrotechnic generator.

15

Solutions based on expanding pyrotechnic tubes filled with explosive and placed against the structure to be ruptured, near to a line of weakness formed therein, have also been proposed.

20

On this point, reference may be made for example to document FR-A-2 619 738.

25 This solution is not entirely satisfactory either. This is because it actually leads to a shock level which is too high for certain applications.

30 Document DE-19604410 describes a device comprising a structure placed in tension between two support elements, and a rupture device associated with this structure in tension so as to rupture the latter on demand.

35 In an attempt to improve the situation, present-day studies are tending toward the use of a damper coupled to the cutting device in order to limit the level of mechanical stress applied to the equipment that is to be released.

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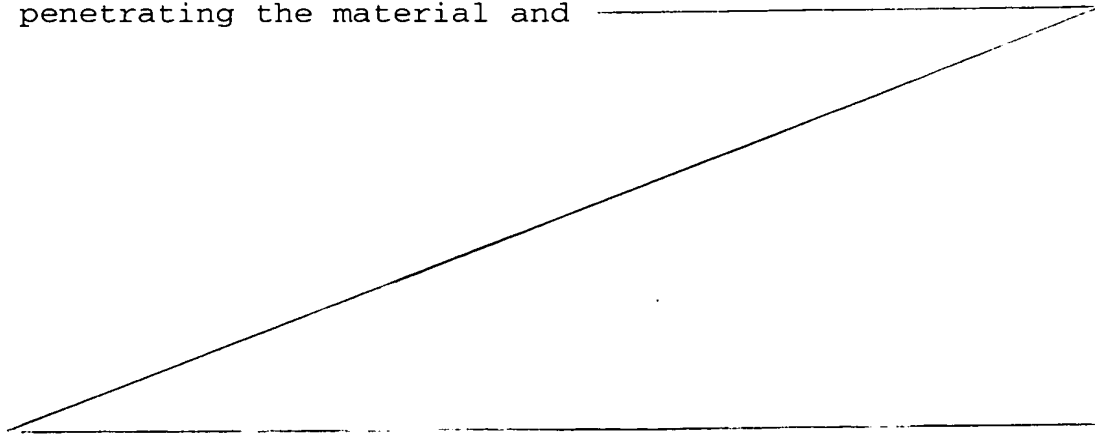
It is an object of the present invention to propose a new device designed to allow the rupture of a structure forming a tie operating in tension and holding a system, which device is designed to limit the mechanical stress applied to the system at the time of the rupture of the tie, particularly to limit the vibration transmitted to the system.

Another auxiliary object of the present invention is to propose a rupture device of a structure avoiding any pollution of the environment.

These objects are achieved in the context of the present invention by virtue of a device as defined in the appended claim 1.

As a preference, this device for the controlled rupture of fibers, particularly pretensioned fibers, is characterized in that it comprises two stressing members arranged one on each side of the fibers, and operating means designed to, on demand, bring about a relative displacement toward each other of the stressing members, the latter being shaped so that, as they move closer together, they impose on the fibers a radius of curvature that is below the threshold of curvature thereof that leads to rupture in bending.

The applicant company has determined that this device, which works by bending the fibers rather than by penetrating the material and



stationary, while the other can move under the actuation of the operating means.

According to an advantageous feature of the present invention, the operating means comprise a pyrotechnic charge capable of generating a high-pressure gas and an inflatable sealed member connected to the pyrotechnic charge and in contact with at least one of the stressing members so as to bring about a displacement of this when said charge is initiated.

According to another advantageous feature of the present invention, the structure to be ruptured, formed on the basis of fibers, may at least in part be agglomerated with a synthetic material so as to form a composite material. As a preference, the structure to be ruptured consists of a strap or the like.

The present invention also relates to an equipment item employing such a rupture device. As indicated above, such an equipment item may, for example, be configured to act as a temporary support for microsatellites on board a rocket, so as to release these at a determined and controlled point on the rocket trajectory.

According to the present invention, an equipment item such as this comprises a structure placed in tension between two support elements, a rupture device free of mechanical shock associated with this structure in tension so as to rupture the latter on demand, and a beam working in compression, inserted between these two support elements in parallel with the structure to be ruptured. In such an equipment item, the beam makes it possible to maintain the relative position of the support elements, in combination with the structure in tension. Further, all that is required is for this structure in tension to be ruptured in order to eliminate the link there is between the two support elements and thus release at least one of these

together with the systems, such as satellites, linked to it.

5 An equipment item such as this may in particular find an application in the support of (a) microsatellite(s) on a launcher. However, it is not restricted to this particular application.

10 Other features, objects and advantages of the present invention will become apparent upon reading the detailed description which will follow and from studying the appended drawings, given by way of non-limiting examples, and in which:

15 - Figure 1 depicts a diagrammatic view in exploded perspective of the basic means that make up a rupture device according to the present invention,

20 - Figure 2 depicts a view in cross section of the same means,

- Figure 3 depicts a view in section of controlled-rupture support equipment comprising a means that can withstand compression,

25 - Figure 4 depicts a detail view of such an equipment item, for the region referenced IV in figure 3, and

30 - Figures 5 to 16 illustrate alternative forms of embodiment of the rupture device according to the present invention.

35 The appended figures 1 and 2 show the basic structure of a device according to the present invention, designed for the controlled rupture of a structure formed of a tape 10.

This tape 10 may itself be embodied in numerous ways.

In the context of the present invention, the structure 10 to be ruptured is preferably formed on the basis of fibers, such as carbon fibers, glass fibers, aramid fibers for example, or alternatively any other type of
5 fiber, used in particular in the textile field and capable of withstanding high tensile forces compatible with the intended applications.

If appropriate, these fibers may be agglomerated in a
10 synthetic material, for example rigidly polymerized, to form a structure to be ruptured 10 made of composite material.

Furthermore, as appropriate, in the context of the
15 present invention, the structure to be ruptured 10 may be nonhomogeneous over its entire length. In particular, it is possible to envisage a structure 10 to be ruptured formed of composite material, that is to say based on fibers embedded in a synthetic material,
20 except in its rupture zone placed facing the stressing means where it consists exclusively of fibers or essentially of fibers and of a small amount of synthetic material.

25 In the context of the present invention, the fibers are oriented essentially longitudinally, that is to say parallel to the direction of the tension exerted on the structure to be ruptured. This may be a unidirectional fiber structure. However, in an alternative form,
30 fibers oriented transversely may be envisaged.

The structures to be ruptured may be formed of a woven or of a nonwoven.

35 As a preference, in the context of the present invention, the structures 10 to be ruptured have a longitudinal elastic modulus in excess of 20 000 MPa.

Furthermore, according to a nonlimiting feature of the invention, the fibers used preferably have an individual diameter of between 0.1 and 25 μm , or even between 0.1 and 10 μm .

5

According to the preferred embodiment of the invention, the aforementioned stressing members are formed of retaining means 20, such as an anvil, and of a punch 30.

10

Further, these stressing means are associated with means 40 designed to bring about a relative displacement, on demand, between the retaining means 20 and the punch 30. The means 40 are preferably of

15

pyrotechnic type.

As mentioned earlier, the stressing members such as the punch 30 and the retaining means 20 are arranged one on each side of the fibers 10.

20

As also mentioned earlier, the stressing members, such as the punch 30 and the retaining means 20, are shaped so that, as they move closer together, they impose on the fibers 10 a radius of curvature that is below the threshold of curvature thereof that leads to rupture in bending.

25

The punch 30 is preferably formed of a hard material, for example high-carbon steel such as 100C6, with a modulus σ_e higher than 2 000 MPa. The punch may be configured in many ways.

30

As a preference, it essentially comprises, on one side, a dihedron formed of two flat faces 32, 34 which meet at a somewhat rounded edge 33 directed toward the structure 10 to be ruptured and, on the other side, a flat face 36 perpendicular to the plane of symmetry of the dihedron and designed to be stressed by the means 40. The edge 33 extends at right angles to the

35

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longitudinal direction of the fibers. The flat face 36 extends parallel to the longitudinal direction thereof.

5 In the context of the present invention, the dihedron formed by the faces 32, 34 preferably defines an angle of between 30 and 90°, very preferably of the order of 60°.

10 The radius of curvature of the rounded edge 33 is preferably smaller than the minimum radius that the fibers 10 can tolerate before they rupture in bending.

15 In the context of the present invention, the means 40 for bringing about the displacement of the punch 30 are advantageously formed by the combination of a high-pressure gas pyrotechnic generator 50 and of an inflatable sealed element 60.

20 The pyrotechnic generator 50 is placed in a rigid casing 52, preferably remote from the punch 30. The rigid casing 52 may itself be formed by assembling several components.

25 The separation between the pyrotechnic generator casing 52 and the punch 30 is intended to mechanically decouple the pyrotechnic generator 50 and the punch 30 so as to avoid the transmission of detrimental mechanical stresses, particularly vibration, between the casing 52 and the punch 30.

30 By way of nonlimiting example, it is possible to envisage a separation of the order of 100 mm, minimum, between the pyrotechnic generator 50 and the punch 30.

35 The structure of the pyrotechnic generator 50 is known per se. The casing 52 defines an internal chamber 54 accommodating a powder charge in conjunction with an initiator 56.

The initiator 56 is preferably of electrical type. However, as appropriate, it is possible to envisage a percussive initiator because of the mechanical decoupling defined between the casing 52 and the punch 30.

It is important that, in the context of the present invention, the powder 54 be designed to generate a gas by combustion and not at all by a deflagration or detonation effect.

The inflatable sealed element 60 is preferably formed of an elongate tube, packaged at rest in the flattened state. Thus, at rest, the flat two main faces of the flattened tube 60 run parallel to the rear attack face 36 of the punch 30 as can be seen in figure 2. One of the flat main faces of the flattened tube 60 incidentally rests on this flat attack face 36. The other face of the tube 60 rests on a stationary bearing face 71.

More specifically still, in the context of the present invention, the inflatable sealed element ~~40~~⁶⁰ is preferably formed of a stainless steel tube.

The sealed connection between the tube 60 and the pyrotechnic gas generator 50 may be achieved by any appropriate means, for example by crimping.

The opposite end of the tube may be plugged by any appropriate means.

By way of nonlimiting example, the inflatable sealed tube 60 may have a diameter of the order of 4 mm and a wall thickness of the order of 0.2 to 0.3 mm.

Those skilled in the art will readily understand that, when the generator 50 develops a pressurized gas inside the tube 60, the tube changes from its flattened rest

state to an inflated state of approximately circular cross section.

Thus, the deformation of the inflatable tube 60 bearing
5 against the surface 71 causes the punch 30 to move against the structure to be ruptured 10, so that the latter is sandwiched between the two stressing members such as the punch 30 and the anvil 20.

10 As already stated, in the context of the present invention, the punch 30 is preferably designed to rupture the element to be ruptured 10, not at all by penetrating the material of which this structure to be ruptured 10 is made and therefore by gradually reducing
15 the thickness thereof, but by local deformation of the fibers of which the structure to be ruptured is made, in bending beyond their ability to deform.

To do that, the anvil 20 is preferably formed of a
20 material not as hard as the punch 30, so as to tolerate at least a slight penetration of the structure to be ruptured 10 and possibly of the punch 30, under the effect of the stress thereon, so as to bring about the aforementioned bending.

25 By way of nonlimiting example, the anvil 20 may be formed of a medium-carbon steel. However, many other materials may be envisaged, including, for example, materials based on elastomer or materials exhibiting
30 plastic behavior, such as aluminum, copper, lead, etc.

By way of nonlimiting example, the anvil 20 may be made of a material having an ultimate tensile strength σ_e of below 600 MPa.

35 As appropriate, the anvil 20 may also have, facing the edge 33 of the punch 30, a groove or hollow making it easier to bend the tape, when the latter rests on the margins of said groove or hollow, while the

intermediate segment of the structure to be ruptured 10 enters said groove or hollow under the effect of the punch.

- 5 If appropriate, the retaining means 20 may incidentally be formed simply of two supports 22, 24 situated on the opposite side of the fibers 10 to the punch 30, as can be seen in figure 14, the two supports 22, 24 being arranged one on each side of the edge 33 of the punch
10 30 in the longitudinal direction of the fibers 10.

According to another advantageous feature of the present invention, the distance separating the two supports 22, 24 is between one times the diameter or
15 thickness of the fibers 10 and the amplitude of relative displacement of the stressing means 20, 30, preferably between two times the diameter or thickness of the fibers 10 and the amplitude of relative displacement of the stressing means 20, 30.

20 Figure 15 illustrates an alternative form of embodiment whereby the stressing members comprise a recessed punch 30, placed facing an anvil 20 which is not as hard, for example based on elastomer.

25 Figure 16 illustrates another alternative form of embodiment whereby the two stressing members are formed of comb-shaped members placed facing each other and offset from one another by half a pitch in the
30 longitudinal direction of the fibers.

When the fibers 10 are stressed in bending by the stressing members 20 and 30, the part of the fibers that lies on the inside of the curvature experiences
35 compressive stress. Conversely, the part of the fibers situated on the outside of the curvature experiences a tensile stress σ_1 due to bending, to which is possibly added a tensile force σ_2 applied to the fibers independently of any bending.

The maximum permissible stress that the fibers 10 can withstand before they rupture can be determined by the relationship:

5 $\sigma = [(d/2)E]/r$

terming:

- . σ represents the maximum local tensile or compressive stress ($\sigma = \sigma_1 + \sigma_2$),
- . E the longitudinal elastic modulus,
- 10 . r the mean radius of curvature, and
- . d the diameter or thickness of the beam consisting of a fiber 10.

15 The applicant company has moreover determined that the above formula led to the following radii of curvature r upon rupture for a fiber having a diameter d of 10 μm :

	E (in GPa)	σ (in MPa)	r (in mm)
High-modulus carbon	3 600	2 400	0.75
High-strength carbon	260	3 200	0.4
R-glass	85	3 200	0.13
E-glass	74	2 450	0.15
Kevlar 49	132	3 000	0.22
Kevlar 29	82	3 000	0.13
Steel (35 NCD 16)	220	1 600	0.68

20 Thus, the applicant company determined that the maximum radius of the edge 33 of the punch 30 is preferably of the order of 1 mm, preferably at maximum of the order of 0.75 mm.

25 As a preference, in the context of the present invention, means designed to initially keep the punch 30 away from the structure 10 to be ruptured as long as the generator 50 is not initiated are also preferably provided.

Such temporary keeping means may be formed of numerous appropriate structures.

5 In the context of the present invention, such temporary keeping means may be formed of two strips of elastic material, for example of silicone elastomer 37, 38, arranged respectively between the structure to be ruptured 10 and one of the flanks 32, 34 of the punch.

10 By way of nonlimiting example, these may be two silicone elastomer strips with a diameter of the order of 2.5 mm.

15 In the context of the present invention, such temporary keeping means may be designed, for example, to keep the edge 33 of the punch 30 a distance of the order of 0.5 mm away from the structure to be ruptured 10.

20 In order to rupture the structure 10, the tube 60 has to receive about 2.5 cm³ of gas at 500 bar.

Thus, the generator 50 is preferably designed to produce at least 1.25 l of gas at one atmosphere.

25 The applicant company obtained very satisfactory results during tests on the severing of an omnidirectional carbon-fiber strap of the order of 25 mm wide and of the order of 0.3 mm thick. These tests, performed with a rupture device of the type illustrated
30 in the aforementioned figures 1 and 2, actually led to a level of shocks on the structure to be ruptured 10 and on its environment of less than 40 g.

35 The device further comprises means 70 designed to keep the inflatable tape 60 in position and to guide the punch 30 between a retracted position away from the structure to be ruptured 10, as illustrated in figure 2, and a working position in which the edge 33 of the punch 30 stresses the structure to be ruptured

10 to bring about local bending thereof and cause it to rupture.

These means 70 supporting the tape 60 and guiding the
5 punch 30 may be embodied in numerous alternative ways.

According to the embodiment illustrated in figures 1 and 2, such support means have thus been represented in the form of a block 72 having a stepped groove.

10

The structure of an equipment item employing such a rupture device will now be described with reference to the appended figures 3 and 4. As indicated earlier, such an equipment item may, for example, be configured
15 to act as a temporary support or interface for micro-satellites on board a rocket or a launcher, so as to release these at a determined and controlled release point.

20 According to the present invention, such an equipment item comprises a structure 10 placed in tension between two support elements 100, 110, a rupture device 20, 30, 40, 50 free of mechanical shock associated with this structure in tension 10 so as to rupture the latter on
25 demand, and a beam 150 working in compression, inserted between these two support elements 100, 110 in parallel with the structure to be ruptured 10. In such an equipment item, the beam 150 makes it possible to maintain the relative position of the support elements
30 100, 110, in combination with the structure in tension 10. Further, all that is required is for this structure in tension 10 to be ruptured in order to eliminate the link there is between the two support elements 100, 110, and thus to release at least one of these,
35 together with the systems, such as satellites, linked to it.

The structure illustrated in the appended figures 3 and 4 is an annular structure centered about an axis O-O.

This structure comprises two mutually parallel washers 100, 110 taking the place of the aforementioned support elements, the mean plane of which is perpendicular to the axis O-O and which are centered on this axis.

The lower washer 10 can rest, for example, on a base, such as the chassis of a satellite launcher, while the upper washer 100 itself acts as a support bracket for these satellites, or for any other equivalent equipment that is to be released with precision at a controlled moment.

The two washers 100, 110 are joined together by a structure 10 working in tension. Furthermore, an element or beam 150 working in compression is inserted between these washers 100 and 110, in parallel with the structure in tension 10.

The structure to be ruptured 10 is associated with a shock-free rupture device schematically depicted in figure 3 and identified by the general reference D, according to the present invention, comprising stressing members 20, 30 arranged one on each side of the structure 10, for example in the form of a punch 30 associated with a pyrotechnic generator 50 and with an inflatable sealed member 60 as indicated earlier.

As indicated earlier, in this context, all that is required is for the structure 10 to be ruptured by implementing the stressing members 20, 30 in order to disconnect the washers 100, 110 and thus release the elements, such as microsattelites, carried by the washer 100.

In the context of this application, the structure to be ruptured 10 may be formed of a continuous annulus centered about the axis O-O (in which case, a set of punch segments 30 covering almost the entirety of the

interior surface of this structure to be ruptured 10 is provided) or of several elements distributed about the axis O-O (in which case a punch 30 covering the width of each structure to be ruptured 10, facing a
5 respective one of these structures, is provided).

It will be noted that the element 10 to be ruptured working in tension and the element 150 working in compression preferably run parallel to the central axis
10 O-O.

The structure to be ruptured 10 is secured, by one of its axis ends, to one of the washers, for example the washer 100, and is secured at its other end to a flange
15 12 designed to be fixed by any appropriate means, for example by screwing, to the other washer, such as 110.

For its part, the element working in compression is formed of a wall or beam built into at least one of the washers 100, 110, such as the washer 100, so as to be
20 able to be separated therefrom when the structure to be ruptured 10 is ruptured. According to the particular embodiment illustrated in figures 3 and 4, the element working in compression 150 is formed of an aluminum
25 cylinder, the inner and outer faces of which are delimited by mutually parallel generators parallel to the axis O-O. The wall 150 is formed integrally with the lower washer 110 and built into the upper washer 100.

30 The geometry whereby the wall 150 working in compression is built into the upper washer 100 may be embodied in numerous alternative ways.

35 According to the nonlimiting embodiment given in the appended figures, the washer 100 has an annular groove 102 defined by a base surface 103 in the form of a ring perpendicular to the axis O-O and centered on the latter, defining the bottom of a groove, and two flanks

104, 105 diverging from one another in the direction away from the base surface 103, and toward the outer surface of the washer 100. The two flanks 104, 105 are preferably symmetric with respect to a generator
5 parallel to the axis O-O and are inclined with respect to this generator by an angle of between 10 and 60°.

The end of the wall 150 working in compression has a geometry that complements this groove 102.

10

Of course, as an alternative, it is possible to provide a partition 150 working in compression and connected by any appropriate means to the base washer 110.

15 By way of nonlimiting example, the wall 150 working in compression may be made of aluminum, with a thickness of the order of 5 mm and a height (distance separating the two washers 100, 110) of the order of 80 mm, the inside diameter of the washers 100, 110 being of the
20 order of 230 mm.

Figure 5 illustrates an alternative form of embodiment whereby the element 70 forming a guide for the inflatable tube 60 and the punch 30 is fixed to the
25 washer 110, while the anvil 20 consists of the element 150 taking the place of the element resistant to compression. More specifically still, the anvil 20 is formed at an additional thickness of this element 150.

30 Like the embodiment of figures 3 and 4, the element 150 resistant to compression is arranged radially on the outside of the element 10.

One of the ends of the structure 10 to be ruptured is sandwiched between the part 70 acting as a guide and
35 the washer 110. The other end of the structure to be ruptured 10 is fixed by any appropriate means to the second washer 100.

Figure 6 illustrates an alternative form of embodiment whereby the structure 10 to be ruptured is formed of a composite piece, equipped with additional thicknesses at each of its ends to form flanges 12, 14 intended for
5 attachment to the washers 110, 100 or any equivalent means.

More specifically still, according to the embodiment illustrated in figure 6, the composite piece comprises,
10 on the ends of the element to be ruptured 10 which typically is formed of a cylindrical skirt, respective flanges 12, 14 which on the whole are perpendicular to the axis of the cylindrical element 10 and face respectively, in the case of the flange 12, inward and,
15 in the case of the flange 14, outward.

The alternative form thus described with reference to figure 6 is made up of a cylindrical element 10 and of two annular flanges 12, 14. According to another
20 alternative form, it is possible to envisage an element to be ruptured 10 formed of a straight tape equipped, at each of its ends, formed integrally, with additional thicknesses 12, 14 similar to the means illustrated in figure 6.

25 The piece 70 acting as a guide for the inflatable tube 60 and for the punch 30 can be formed integrally on the flange 12 or attached and secured to the latter by any appropriate means.

30 Figure 7 illustrates another alternative form whereby the compression element 150 acts as a guide for the punch 30 and for the inflatable tube 60. In this case, there is an anvil 20 on the opposite side of the
35 element 10 to be ruptured to the punch 30. This anvil 20 is fixed, by any appropriate means, to one of the flanges or washers 100, 110.

More specifically still, according to the embodiment illustrated in figure 7, the element 150 resistant to compression is equipped within its mass with a groove which guides the inflatable tube 60 and the punch 30.

5

By contrast, according to the alternative form illustrated in figure 8, the inflatable tube 60 and the punch 30 are placed in a guide 70 attached to the element 150 resistant to compression. Furthermore, here again, according to figure 8, there is an anvil 20 on the opposite side of the element to be ruptured 10 to the punch 30. It is furthermore possible to envisage for the anvil 20 to itself be secured to the guide 70.

10

Yet another alternative form, illustrated in figure 9, consists in placing the anvil 20, formed of an attached part, on the element 150 resistant to compression, and the guide 70 on the opposite side of the element to be ruptured 10 to the anvil.

15

In the various embodiments described above, with reference to figures 3 et seq., the element to be ruptured 10 runs in an overall direction parallel to the axis O-O of the annular structure. Further, the punch 30 is mounted to move in a direction generally transversal to this axis O-O.

20

Furthermore, it was indicated earlier that the element to be ruptured 10 could be formed either of a continuous annular structure centered about the axis O-O, or of discrete elements distributed about this axis O-O.

25

In this context, the element to be ruptured 10 may be formed, for example, of a tape. This may be unitary, that is to say formed of a single strand, for example of elongate rectilinear cross section, or alternatively circular or oblong, or may be split into various strands.

30

35

According to another alternative form, the element to be ruptured 10 may be formed of a tubular tape or equivalent, that is to say one having a loop-shaped cross section, for example in the form of a closed curve. In this case, it may, for example, be a flattened circular knit.

In the latter cases, it is possible to envisage placing at least one of the anvil elements or punch 30 in the space between the various strands making up the element to be ruptured or even in the interior space of the cross section of a tubular tape.

Figure 10 thus illustrates a support structure in the shape of an ogee 70 placed between two strands 18, 19 of an element 10 to be ruptured, and acting as a guide for the portions of inflatable tube 60 and for the punch segments 30 which are placed facing complementary anvils 20 so that the strands 18, 19 are sandwiched between said anvils 20 and the punch segments 30.

When such an ogee shape 70 is placed inside the cross section of a tape 10 which has a cross section in the form of a closed curve, it is of course necessary for the ogee shape 70 to support a number of portions of inflatable tube 60 and of punch 30 which together cover the entire periphery of the element to be ruptured 10.

According to the embodiment illustrated in figure 10, the various portions of inflatable tube 60 and punch segments 30 are located overall in a common plane orthogonal to the axis of the tape 10. As an alternative, however, particularly when the punch segments 30 have to cover the entire periphery of the ogee shape 70, it is possible to envisage staging these longitudinally along the ogee shape 70 to ensure an overlap between the ends of the various punch segments 30 and thus guarantee complete rupture of the tape 10.

Figure 11 illustrates a reverse arrangement, that is to say an anvil 20 formed of an ogee shape located at the center of the tape to be ruptured and structures 70
5 providing guidance of the inflatable tube 60 and of associated punch segments 30 arranged facing it, on the outside of the element to be ruptured 10.

In the context of figure 10, it is possible to envisage
10 arranging the pressurized gas pyrotechnic generator on the outside of the ogee shape 70 and of the structure to be ruptured 10. However, as has been illustrated in figure 12, as an alternative, it is possible to envisage incorporating the pyrotechnic generator 50
15 into the ogee shape 70. In this case, use may be made of a pyrotechnic generator 50 common to the various punch segments 30 or alternatively of a pyrotechnic generator 50 associated with each respective punch 30.

20 Figure 13 illustrates another alternative form of embodiment whereby there are two punches 30 each associated with a respective pyrotechnic generator (not depicted in figure 13 in order to simplify the illustration) facing each of the zones to be severed of
25 the element 10. Of course, a correspondingly designed facing anvil 20 is provided.

This arrangement illustrated in figure 13 allows a redundant effect and a guarantee of rupture of the
30 structure in the event of deficiency of one of the pyrotechnic generators 50 or alternatively of the associated sealed inflatable tube 60 or even of the displacement of the punch 30.

35 The use of such a double structure of punch 30 can be applied to all the alternative forms of the present invention which have already been described.

